

S. S. "MIELERO"

Inertia of Section in way of  
oil tank.Base as Axis.

Item & Scantlings.	Area sq. ins.	Lever in ft.	A x h.	A x h <sup>2</sup>	d.	Ad <sup>2</sup> 12
$\frac{1}{2}$ kl. plate 23 $\frac{1}{2}$ " x 1.02	23.96	—				
shl. 24' x 12 x .60	172.80	.2	34	7	.41	2
" 72" x .60	43.20	2.25	97	219	3.41	42
F.G.H.T. 24' x 12 x .64	184.30	14.9	2746	40910	22.7	7913
K. 51 x .66	33.66	28.0	942	26390	4.25	51
L. 47 x .76	35.72	31.6	1130	35670	3.9	45
U.Dk.stringer 62 $\frac{1}{2}$ x .54	33.75	32.6	1100	35860		
U.Dk. 277 $\frac{1}{2}$ " x .40	111.00	33.2	3685	122360	.7	5
2nd Dk.Str. 78 x .44	34.30	24.1	827	19930		
" " pltg. 88 x .40	35.20	24.3	855	20780		
Expn.trunk side 102 x .42	42.82	28.5	1221	34800	8.5	258
$\frac{1}{2}$ centre line bkd.						
30' x 12 x .184	66.22	18.5	1225	22670	28.5	4482
$\frac{1}{2}$ ctre.klsn. 68" x .21	14.28	2.8	40	112	5.7	38
Margin plate 63 x .48	30.24	4.8	145	700		
Inner bottom 282" x .40"	112.80	4.5	508	2280		
Keel bar 6 x 6 x .58	6.70	—				
5 x 5 x .50	4.75	4.4	21	92		
5 x 5 x .56	5.32	4.9	26	130		
5 x 5 x .50	4.75	24.2	115	2780		
5 x 5 x .43	4.08	24.6	100	2470		
5 x 5 x .60	5.70	32.7	186	6100		
3 $\frac{1}{2}$ x 3 $\frac{1}{2}$ x .43	2.80	33.1	92	3070		
5 x 5 x .50	4.75	33.5	159	5330		
Stringer 1. 17" x .44	7.48	9.7	72	700		
7 x 3 $\frac{1}{2}$ x .62	6.18	9.7	60	580		
2nd. 17 x .44	7.48	14.5	108	1570		
7 x 3 $\frac{1}{2}$ x .62	6.18	14.5	90	1300		
3rd. 17 x .44	7.48	19.3	144	2780		
7 x 3 $\frac{1}{2}$ x .62	6.18	19.3	120	2300		
$\frac{1}{2}$ (15x3 $\frac{1}{2}$ x3 $\frac{1}{2}$ x.52 channel)	5.9	9.7	57	550		
" " " "	5.9	14.6	86	1260		
$\frac{1}{2}$ (12x3 $\frac{1}{2}$ x3 $\frac{1}{2}$ x.50)	4.8	19.2	92	1770		
$\frac{1}{2}$ shelf plate 25 $\frac{1}{2}$ x .20	5.1	25.2	130	3240		
& flange						
3 $\frac{1}{2}$ x 3 x .43	2.6	25.3	66	1660		
	1088.38		16279	400370		12836

C. C. 14.96 ft.above Base.

Moment of Inertia of Section

12836  
 413,206  
 243,466  
 169,740  
 2  
339,480

$$\frac{1}{4} \text{ deck } \frac{339480}{17.54} = 19300$$

$$\frac{1}{4} \text{ Keel } \frac{14.96}{17.54} = 22700$$



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