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|---|--|
| Percent of strength of longest seam: $J = \frac{235 - 36}{235} \times 100 = 84,7\%$ | $3\frac{3}{8}"$ longest stays, 6 threads pr. 1' W.P. = $\frac{(95,72 - 8,6)^2}{520 \times 400} = 15,97 \text{ kg/cm}^2$ |
| Rivets: $J = \frac{36 \times 0,18 \times 5 \cdot 1,875}{49 \times 235 \times 35} \times 100 = 85,2\%$ | $1\frac{1}{2}"$ stay bolts, 9 threads pr. 1' W.P. = $\frac{(93,1 - 6,8)^2}{95 \times 187} = 15,58$ |
| Circum seams: $J = \frac{36 \times 0,18 \times 2 \cdot 1}{49 \times 35 \times 102} \times 100 = 92,0\%$ | $1\frac{1}{2}"$ " " " (Shell) W.P. = $\frac{(93,1 - 6,8)^2}{95 \times 187} = 15,8$ |
| Shell plate: W.P. = $\frac{(35 - 16) \times 34,7 \times 49}{182 \times 4630} = 15,52 \text{ kg/cm}^2$ | $1\frac{3}{4}"$ " " " (Plate) W.P. = $\frac{(44,45 - 6,8)^2}{17 \times 2675} = 16,4$ |
| Front and back in steam space: W.P. = $\frac{(34,5 - 0,8) \times 6900}{520 \times 400} = 15,64$ | $3\frac{3}{4}"$ stay tubes, 8" in thick: W.P. = $\frac{(1402 \times 5,27)}{(2875 \times 220) \times (3 \times 5945)} = 15,6$ |
| Wide water space, front end: W.P. = $\frac{(25,5 - 0,8) \times 3740}{355 \times 220} = 15,86$ | Girders, combustion chambers (center) W.P. = $\frac{(775 - 200) \times 270 \times 775}{310 \times 200} = 16,05$ |
| " " " " " back end: W.P. = $\frac{(25,5 - 0,8) \times 4100}{187 \times 340} = 16,61$ | " " " " " (Side): W.P. = $\frac{(832 - 38 \times 245 \times 2)}{(775 - 200) \times 270 \times 775} = 15,75$ |
| Tube plate, combustion chambers W.P. = $\frac{(25 - 0,8) \times 2740}{275} = 15,52$ | $1\frac{3}{8}"$ stay bolts on top of Comb. Chamb.: W.P. = $\frac{(4762 - 6,8)^2}{530} = 15,59$ |
| Shell " " " " W.P. = $\frac{(21 - 0,8) \times 3600}{202} = 20,2$ | Back end: W.P. = $\frac{(25,5 - 0,8)^2 \times 5083}{433} = 16,22$ |
| Top " " " " W.P. = $\frac{(22 - 0,8) \times 5400}{200 \times 310} = 17,8$ | " " " " W.P. = $\frac{(25,5 - 0,8)^2 \times 6300}{430} = 16,01$ |
| Back " " " " W.P. = $\frac{(19 - 0,8) \times 3600}{187 \times 195} = 16,33$ | |
| Furnaces, Morison W.P. = $\frac{1080 \times (75 \times 0,8)}{935} = 15,9$ | |

| | | |
|--|---|---|
| Heating surface of 326 - 3 $\frac{1}{2}$ " tubes | = | 214,00 m ² |
| " " Combust. Chambers, top & sides | = | 13,30 " |
| " " " tube & backpl. | = | 12,40 " |
| " " x furnaces | = | 16,30 " |
| Total heating surface | = | 2755 m ² = 256,00 m ² |
| Koeff. k = $\frac{2755}{15,25 \times 12,08}$ | = | 0,98 |

Totalt gjennomgangsareal av rør: $A = 1,34 \text{ m}^2$

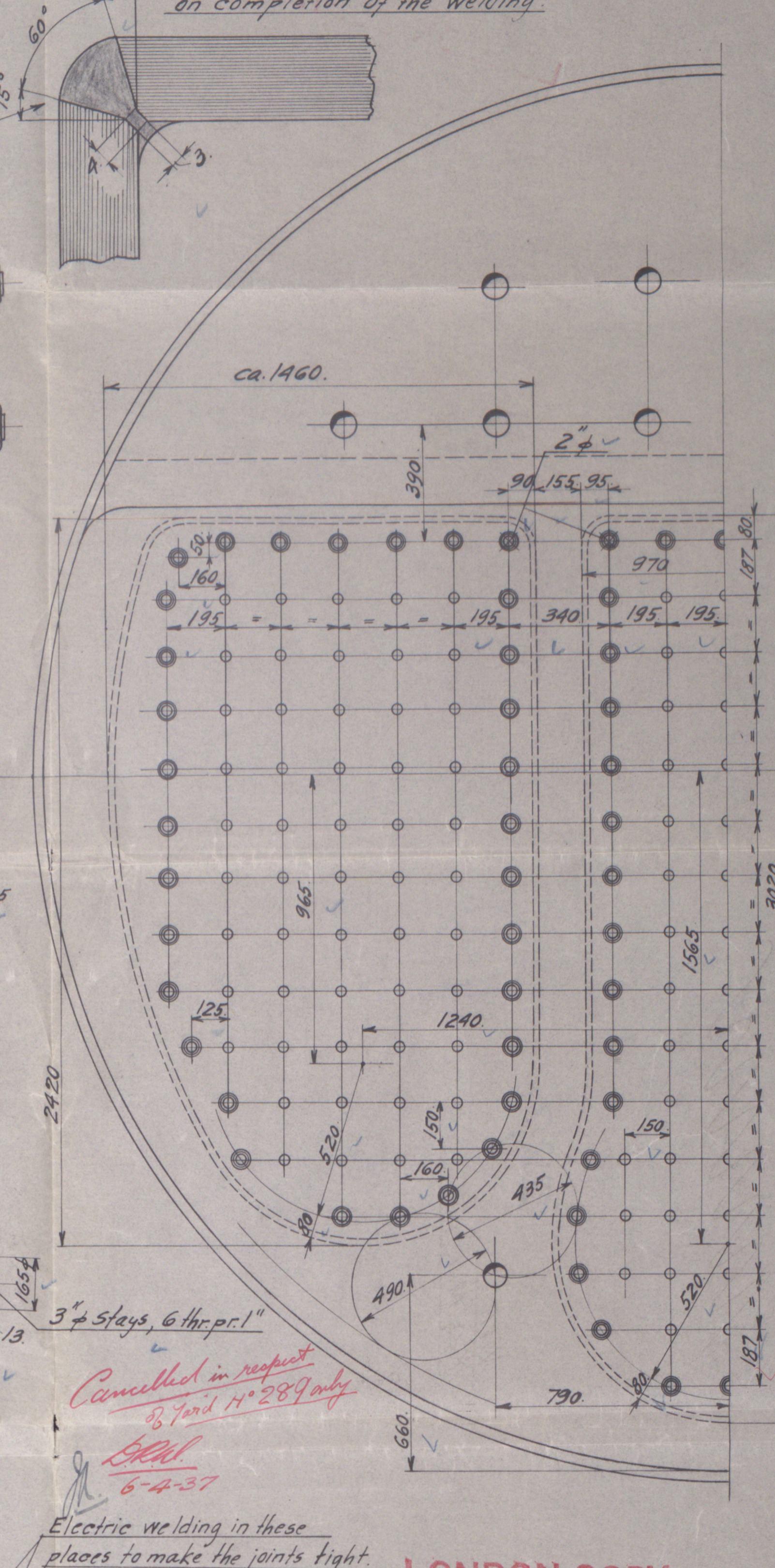
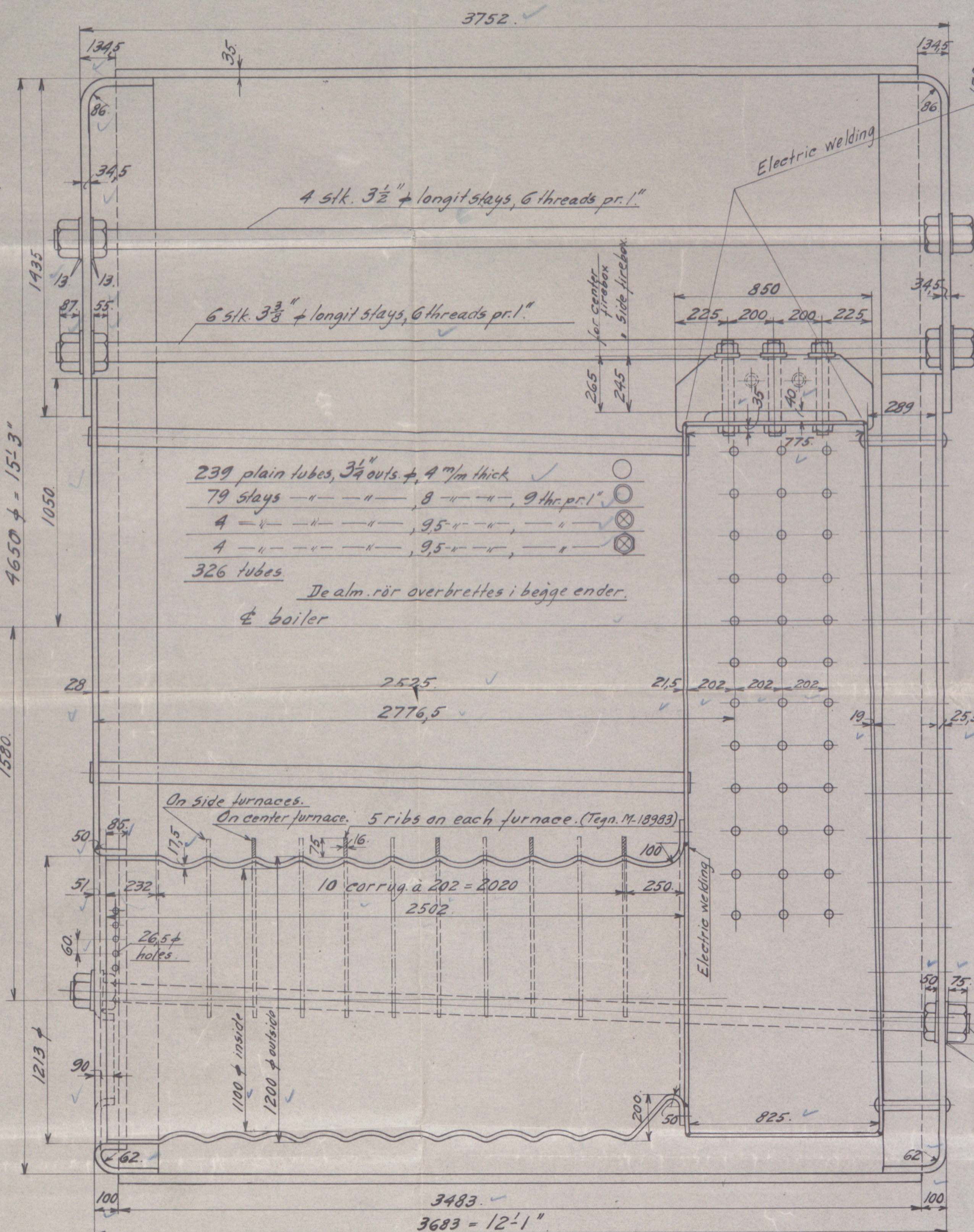
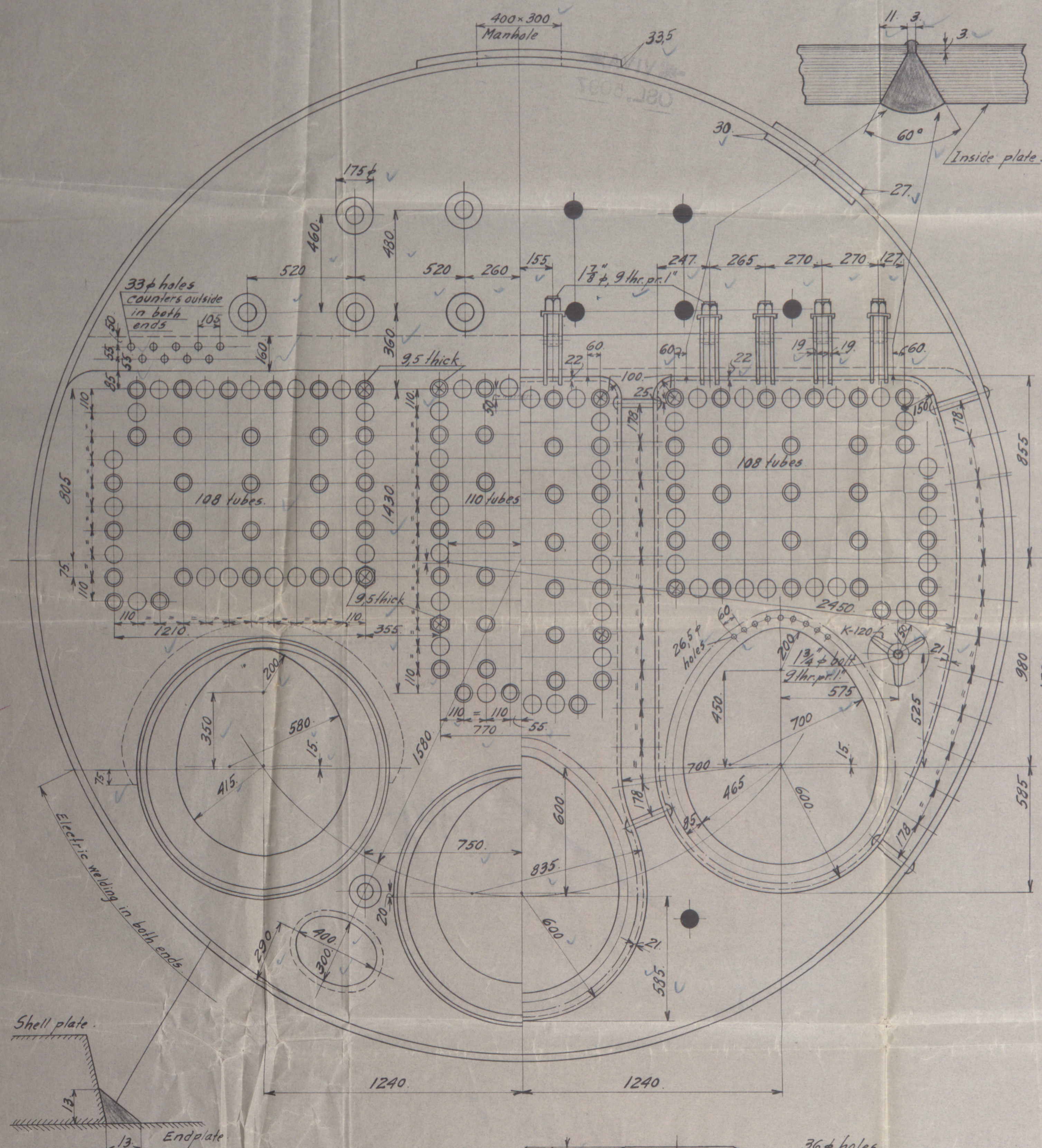
$$\frac{\text{Gjennomgangsareal}}{\text{Ristareal}} = \frac{A}{K} =$$

Totalt ristareal pr kjele =

$$\frac{\text{Hefeflate}}{\text{Ristflate}} = \frac{H}{K} =$$

○ $\frac{1}{2}$ " ϕ stay bolts, 9 threads pr. 1", riveted over in-and-outside.
◎ $\frac{3}{4}$ " ϕ — " — " — " — " — " — "

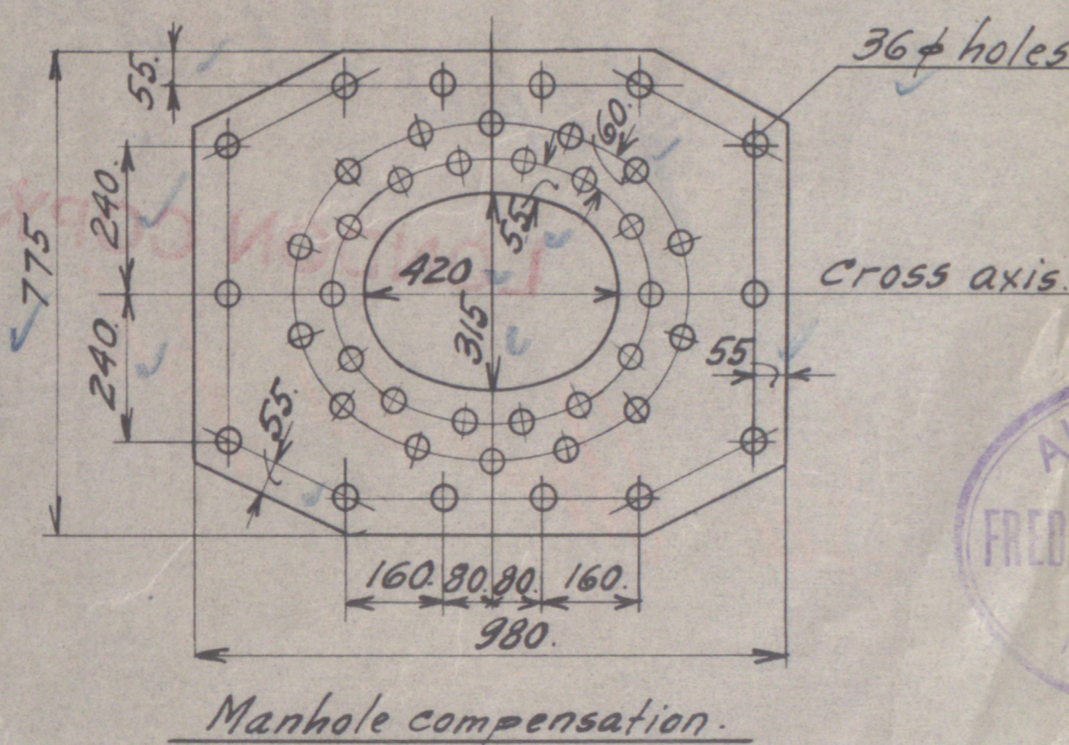
Note:
The combustion chambers to be annealed on completion of the welding.



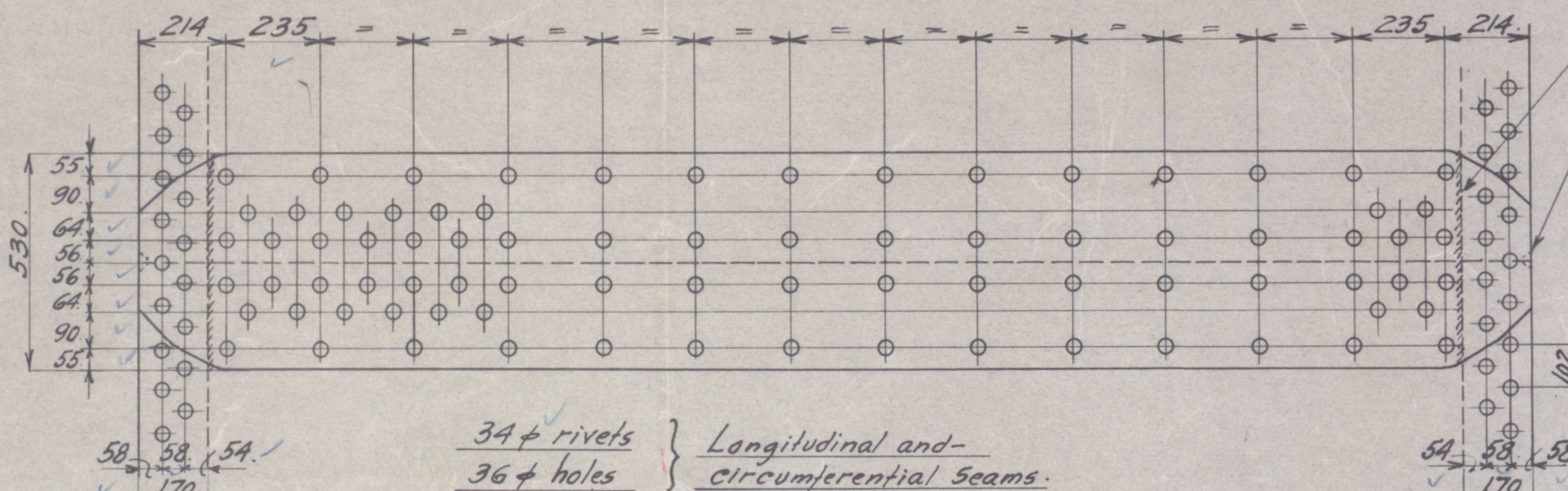
Cancelled in respect
of Ford N° 289 only
OK'd.
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Electric welding in these
places to make the joints tight

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[illegible]

AKTIESELSKABET
 DATO: 24-37
 FREDRIKSSTAD MEK. VERKSTED
 NAVN: M.T.O.
 FREDRIKSSTAD

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M-18948

FIRST AV: Lloyd's

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Amended plan for 289

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