

36635

1/2 RUDOLF 8582

Swedish
Gothenburg 1969 1943
6

Gothenburg
White building
Bretand Larsen

to E of Rudder = 76.475
41'-0" = 12.500
20'-11" = 6.375
4116 tons = 4079 M³

100 AI

= 78.75

6.375

15 8.33 (6.390 - 5.098) 19.31 = 1.208 m.

Moulded Breadth 12.500 m.
Standard R.O.B. 8/50 = 250 m.m.
Ship's R.O.B. = 260
Excess 10

Correction: $\frac{10}{4} \times 3128 = -1$ m.

6.390

Standard height of superm. 1.833
" " R.O.B. 1.224
Deduction for C.S.S. 790

Equ. Poop enclosed
" overhang
R.O.B. Enclosed.

(S)	(S)	Height	Height Correction	(E)
16.781	16.781	2180		16.781
3.744	1.872			1.872
26.230	26.230	1217	1217/1224	26.080

$\frac{S}{Z} = 72.08\%$
 $\frac{S}{Z} = 68.72\%$
 $\frac{E}{Z} = 68.52\%$
no Line A = 60.48%

File enclosed
" overhang

5.550	5.550	2837		5.550
1.220	.610			.610

Tonnage penalty aft
" top of light

1.220	1.224 = diff x 384
.380	.285
55.125	52.552

1.224
Deduction = 790 x 60.48 = -478 m.

891	1	891	230	480	1	480
396	4	1584	15	124	4	496
99	2	198	0	0	2	0
0	4	0	0	0	4	0
198	2	396	0	0	2	0
792	4	3168	2	2	4	8
1782	1	1782	260	260	1	260
		8019				

Mean Actual Sheer aft = Deficient
" Standard

Mean Actual Sheer fwd = Deficient < 50%
" Standard

} Deficient

$\frac{8019 - 1224}{18} (75 - \frac{7208}{2}) = 147$ m.
1775

Tabular Freeboard. 825
 $\frac{7875 + 68}{1.36} = 890$ 890

Depth to R.O. Deck 7.607
1.983
(d) = 5.624
 $\Delta = 4325$ tons
 $T = 21.46$

$\frac{5624}{48} = 117$ m.
51 + 117 = 168 m.
Deduction = $\frac{4325}{40 \times 21.46} = 5.04$ = 128 m.

Depth correction 208
Deduction for superm. 478
Sheer correction 147
R.O.B. correction 1
Deck thickness correction
Height of R.O.D. 1217
1572 479 + 1093 = 1983 m.m.

Raised Quarter 1983 m.m.

245	1738
128	1835
117	1866
117	2100
168	2151

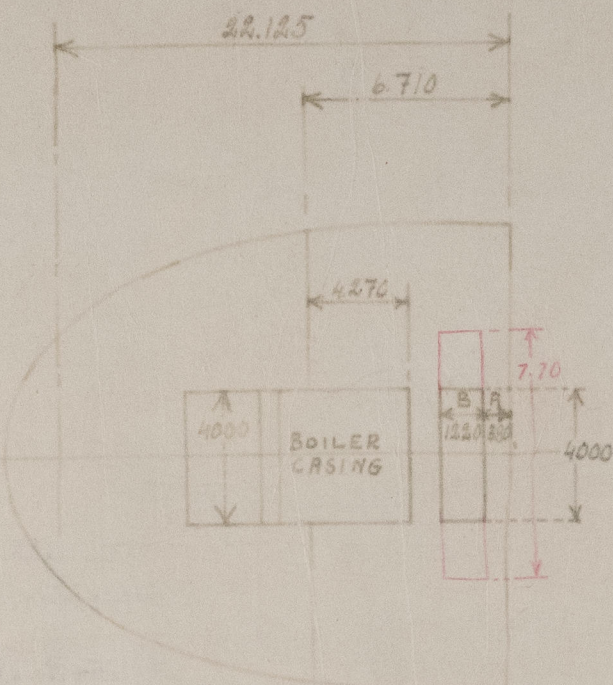
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POOP



Sheers of Upper dk at Poop Front = 0.
 Height of Poop deck at Poop Front = 2180.
 Height of Poop deck above Upper deck:-
 At A.P. = 2660 mm.
 At 1/6 L from A.P. = 2304 mm.
 Virtual Sheers at A.P. = 2660 - 2180 = 480 mm.
 Virtual Sheer at 1/6 L.A. = 2304 - 2180 = 124 mm.

TOTAL LENGTH OF POOP	=	22.125	✓
POOP FRONT TO ACCOM. BHD	=	6.710	✓
		15.415	✓
EQUIV LENGTH OF BOIL. CAS	$\frac{4.270 \times 4.000}{12.500}$	= + 1.366	✓
EQUIV POOP ENCLOSED		16.781	✓
		22.125	✓
LENGTH FROM POOP FRONT TO EQUIV. BHD.	=	5.344	✓
OPENING (A)	=	.380	✓
OF TONNAGE OPENING (B)	=	1.220	✓
		1.600	✓
		5.344	✓
EQUIVALENT POOP OVERHANG (C)	=	3.744	✓
75% (A)	$.75 \times .380$	=	.285
50% (C)	$.50 \times 3.744$	=	1.872
		2.157	

$$\frac{B-b}{B} [(A+B+C) - (.75A + .50C)] = \frac{12.500 - 7.700}{12.500} \left[\frac{5.344 - 2.157}{3.187} \right] = \underline{\underline{1.224.}}$$

Displacements in salt water incl. shell plating.

75% of moulded depth = 3602 tons
 85% " " " = 4149 "
 95% " " " = 4676 "

Tons per inch immersion in salt water.

75% of moulded depth = 20.9
 85% " " " = 21.3
 95% " " " = 21.8

Note.

A.B. Lindholm's Værk, Løkkenburg, Yard No 973
 Peder A.B. Bisfort (G. Harberg, Mgr), Løkkenburg.



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