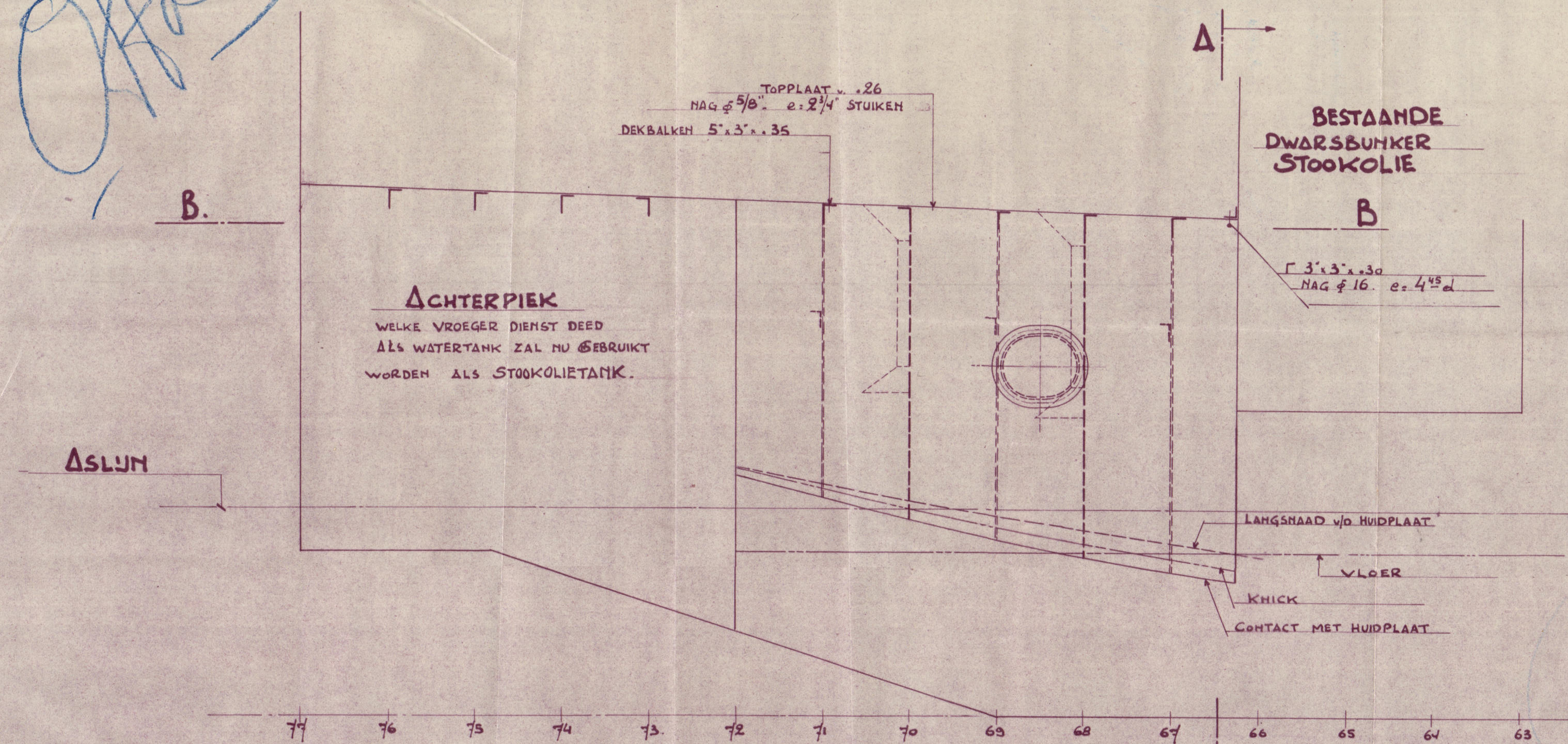
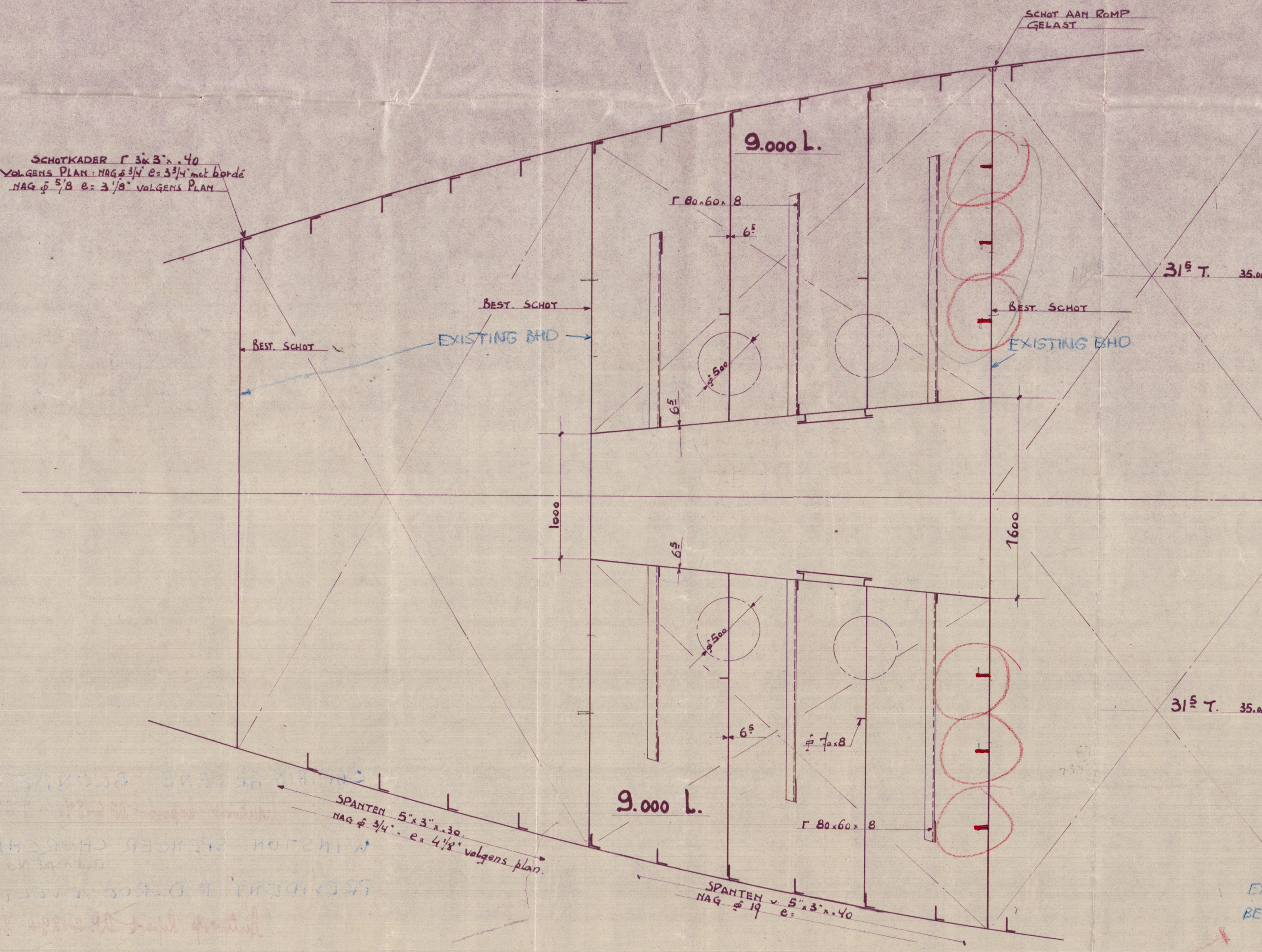


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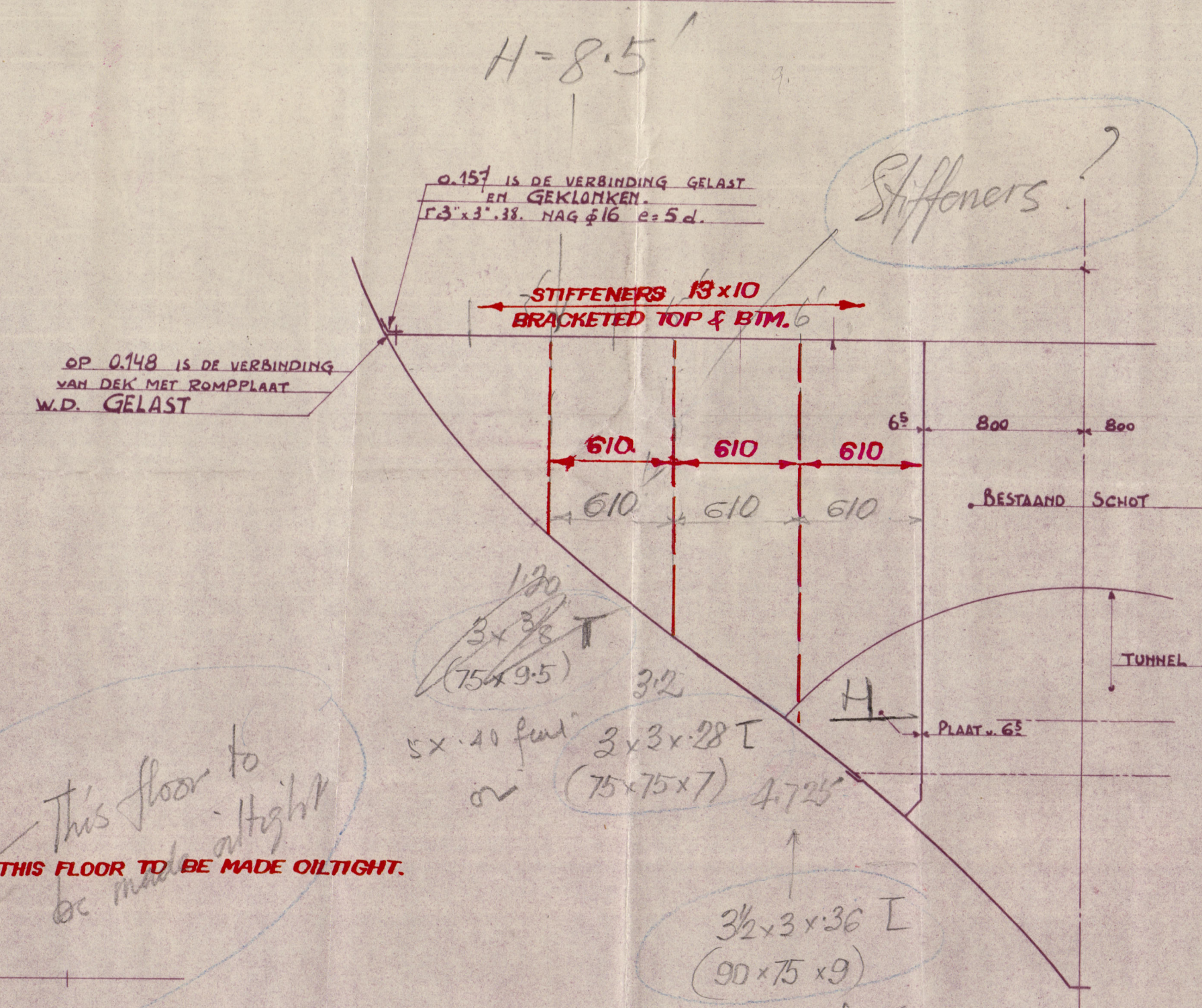
LANGSDOORSNEDE



PLANZICHT B.B.



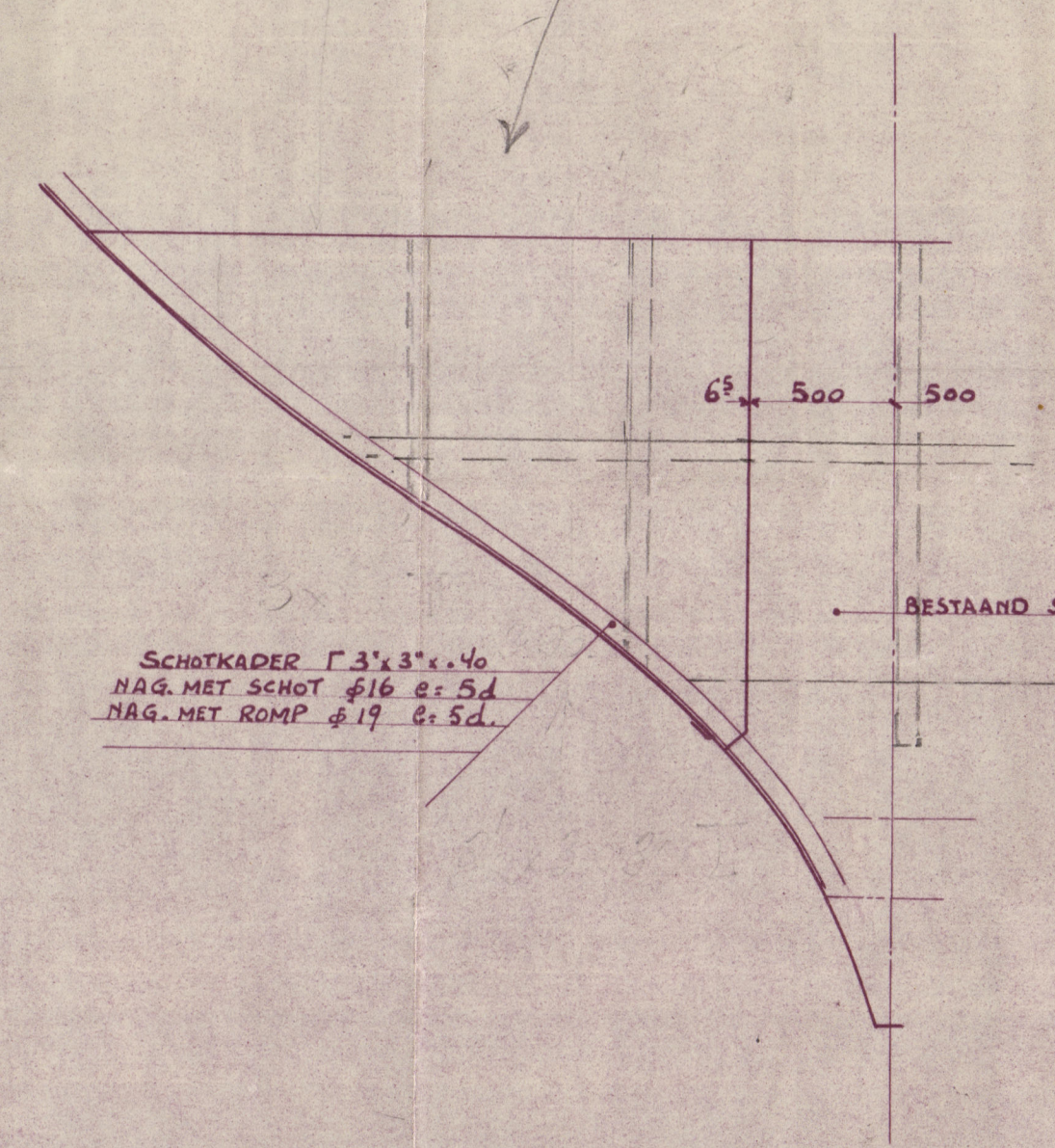
DOORSNEDE Δ.Δ.



SCHOT OP SP. 72.

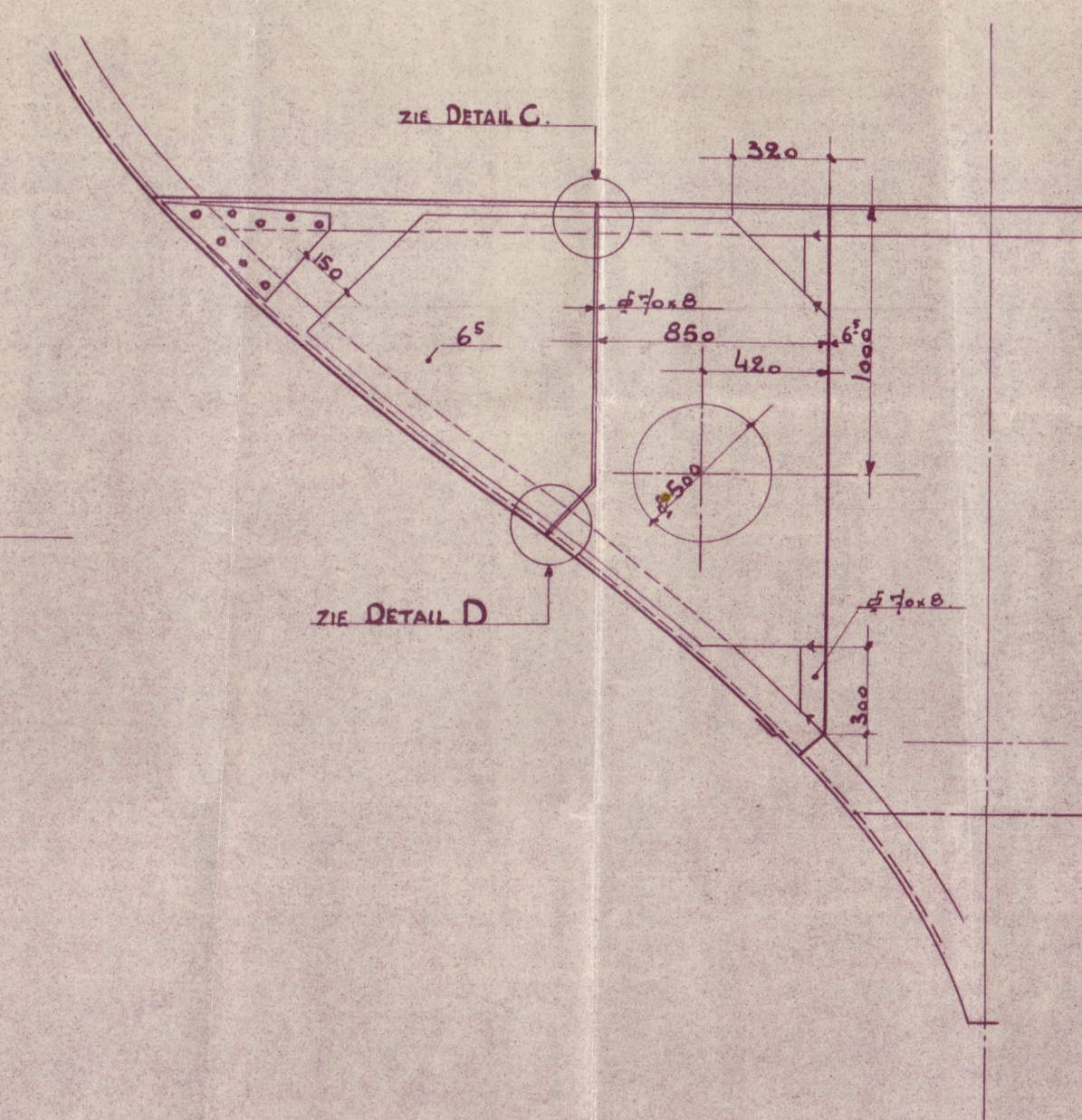
NAAR ACHTER GEZIEH.

H=8.5' (EXISTING BULKHEAD)



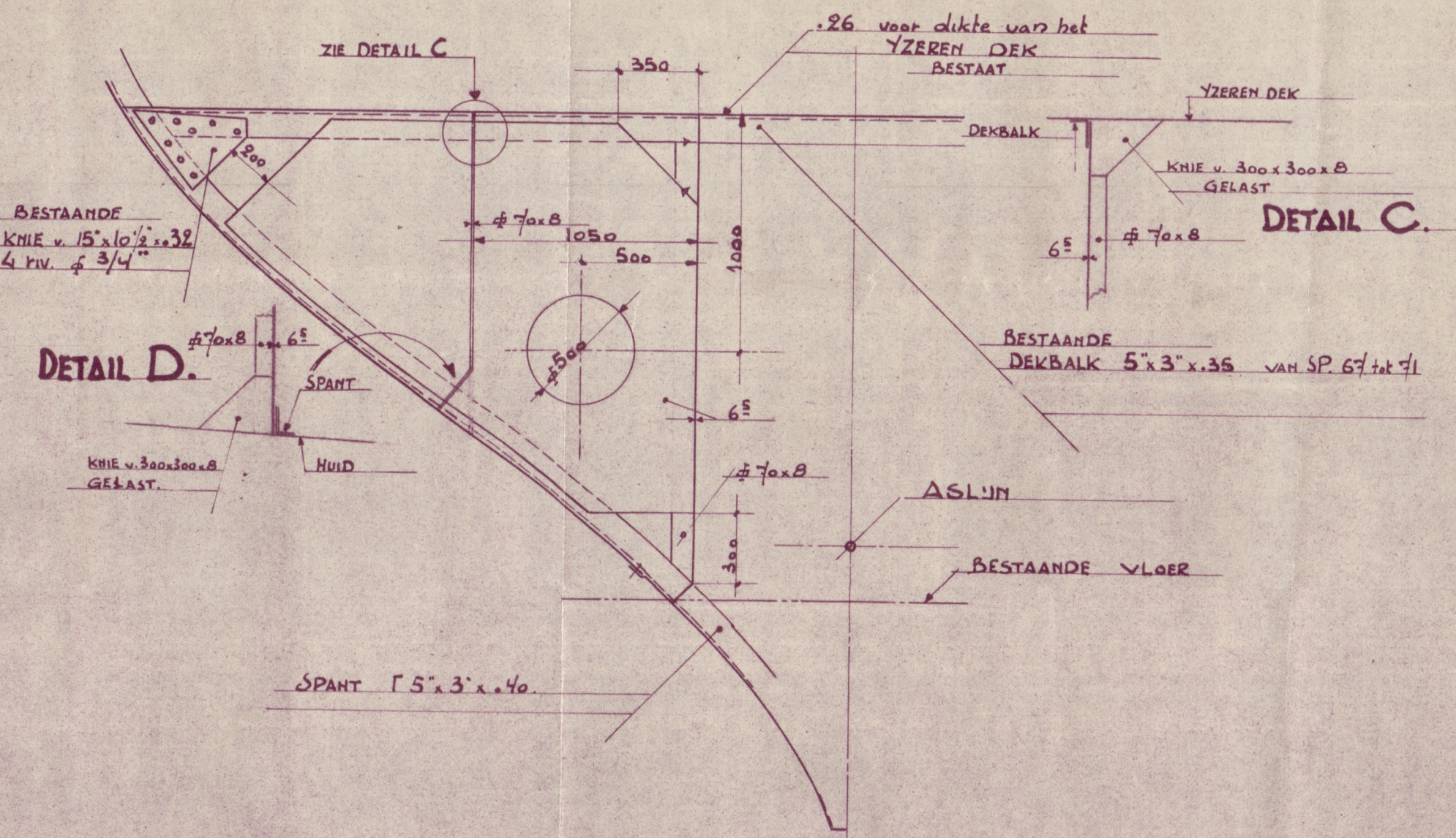
SP. 70. SLINGERSCHOT.

NAAR VOREN GEZIEH



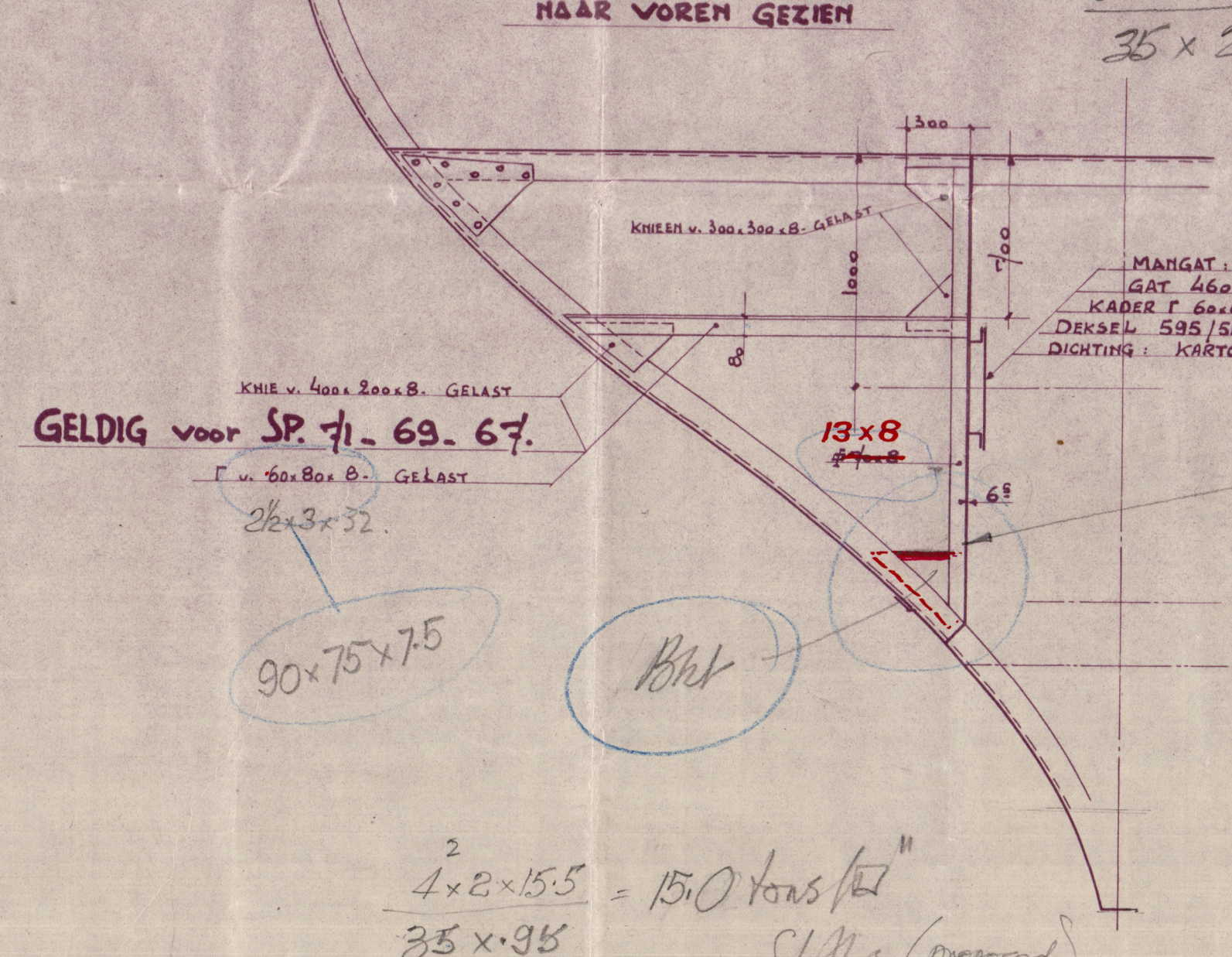
SP. 68. SLINGERSCHOT.

NAAR VOREN GEZIEH



SP. 69.

NAAR VOREN GEZIEH



$$\frac{6.25^2 \times 2 \times 11}{35 \times 293} = 8.35 \text{ tons/l}^2 \text{ Borne}$$

$$\text{Stiffers (Rule)} = 3 \times 3 \times 30 \times \frac{1}{2} \times .99 \text{ (Transverse Rules)}$$

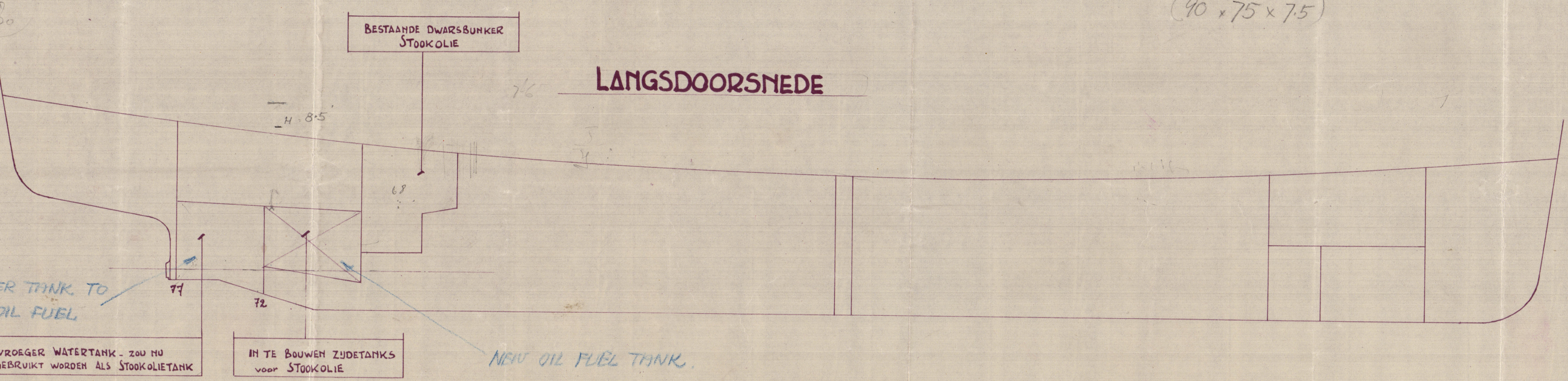
$$(\text{Prop}) = 2 \frac{3}{4} \times 32 \text{ flat} = .95$$

$$\text{Per ship rules } H = 11' 2' 4' \frac{1}{4} = 2.8$$

$$= 3 \times 2 \frac{1}{2} \times 28 \text{ T} \leftarrow 5 \text{ tons/l}^2 \text{ Stress}$$

$$\frac{4 \times 1.75 \times 11}{350} = .88 = \frac{3 \frac{1}{2} \times 3 \times 30}{(90 \times 75 \times 75)}$$

LANGSDOORSNEDE



BESTAANDE NAGELING OP

0.148	0.157
Rompplaten: 1: Langsnaden: 2 rjen nagels φ 19 e. 4 ¹ / ₂ d. 2: Stukken: 2 rjen- φ 19 e. 3 ¹ / ₂ d. 3: Borde met de spanter- φ 19 e. 6 ¹ / ₂ d. 4: Borde met schot r. φ 72 volgens plan φ 19 e. 5 d. Schot r. met schot φ 72 volgens plan φ 16 e. 5 d. Naad van φ 72 φ 16 e. 5 ¹ / ₂ d. Naad v. dwarsbunker φ 16 e. 4 d. Lower deck met dekbalken φ 16 e. 5 d.	Rompplaten: 1: Langsnaden: 2 rjen nagels φ 19 e. 4 ¹ / ₂ d. 2: Stukken: 2 rjen- φ 19 e. 3 ¹ / ₂ d. 3: Borde met de spanter- φ 19 e. 6 ¹ / ₂ d. 4: Borde met schotkader φ 72 volgens plan φ 19 e. 5 d. Schot r. met schot φ 72 volgens plan φ 16 e. 5 d. Naad van φ 72 φ 16 e. 4 ¹ / ₂ d. Naad v. dwarsbunker Gelast Lower deck met dekbalken φ 16 e. 6 ¹ / ₂ d.

ad
S.S. 48

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CAPTAIN ARSENE BLONDE

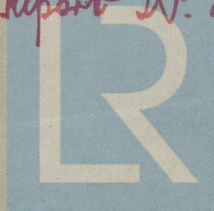
(Antwerp Report No 24891.- 4-48)

WINSTON SPENCER CHURCHILL

Antwerp No. 24908.

PRESIDENT F. D. ROOSEVELT.

Antwerp Report No. 24894-8,48



Lloyd's Register
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