

TIMBER

Lloyd's Register of Shipping.

SURVEYS FOR FREEBOARD.

Index. No. _____
(For London Office only.)

Computation of Freeboard for Steamer, Sailing Ship, Tanker having <u>Roop Bridge and Forecastle</u>					Port of Survey _____
(Type of Superstructures.)					Date of Survey _____
Ship's Name <u>SS "STENSBY"</u>	Nationality and Port of Registry	Official Number	Gross Tonnage	Date of Build	Name of Surveyor _____
Moulded Dimensions: Length Breadth Depth					Particulars of Classification _____
Moulded displacement at moulded draught = 85 per cent. of moulded depth _____ tons					
Coefficient of fineness for use with Tables _____					

Depth for Freeboard (D) Moulded depth Stringer plate Sheathing on exposed deck $T \left(\frac{L-S}{L} \right) =$ Depth for Freeboard (D) = <u>28.03</u>	Depth correction (a) Where D is greater than Table depth (D-Table depth) R = <u>+ 12.65</u> (b) Where D is less than Table depth (if allowed) (Table depth-D) R = If restricted by superstructures	Round of Beam correction Moulded Breadth (B) Standard Round of Beam = $\frac{B \times 12}{50} =$ Ship's Round of Beam = Difference Restricted to Correction = $\frac{\text{Diff}^e}{4} \times \left(1 - \frac{S_1}{L} \right) =$ <u>- .05</u>
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DEDUCTION FOR SUPERSTRUCTURES.

	Mean Covered Length (S)	Equivalent Enclosed Length (S ₁)	Height	Height Correction	Effective Length (E)	
Poop enclosed						Standard Height of Superstructure _____
" overhang						" " R.Q.D. _____
R.Q.D. enclosed						Deduction for complete superstructure <u>38.67</u>
" overhang						Percentage covered $\frac{S}{L} =$
Bridge enclosed						" " $\frac{S_1}{L} =$
" overhang aft						" " $\frac{E}{L} =$ <u>52.09%</u>
" overhang forward						Percentage from Table, Line A.
F'cle enclosed						(corrected for absence of forecastle (if required))
" overhang						Percentage from Table, <u>Line B. TIMBER</u> <u>70.55%</u>
Trunk aft						(corrected for absence of forecastle (if required))
" forward						Interpolation for bridge less than 2L (if required)
Tonnage opening aft						Deduction = <u>38.67 x .7055 = - 27.28</u>
" " forward						
Total						

SHEER CORRECTION.

Station	Standard Ordinate	S M	Product	Actual Ordinate	Effective Ordinate	S M	Product
A.P.		1				1	
$\frac{1}{8}L$ from A.P.		4				4	
$\frac{2}{8}L$ "		2				2	
Amidships		4				4	
$\frac{3}{8}L$ from F.P.		2				2	
$\frac{1}{8}L$ "		4				4	
F.P.		1				1	
Total							

Correction = $\frac{\text{Difference between sums of products}}{18} \left(.75 - \frac{S}{2L} \right) =$ - .89

If limited on account of midship superstructure.

If limited to maximum allowance of $1\frac{1}{2}$ ins. per 100 ft.

Deduction for Tropical Freeboard.

Addition for Winter and Winter North Atlantic Freeboard.

Depth to Freeboard Deck = 28.03
Summer freeboard = 3.78
Moulded draught (d) = 24.25

Deduction for Tropical freeboard and addition for

Winter freeboard = $\frac{d}{4}$ inches = 6.06" = 154.7m

Addition for Winter North Atlantic Freeboard (if

required) = $\frac{d}{3} =$ 8.08" = 205.7m

Deduction for Fresh Water.

Displacement in salt water at summer load water line

$\Delta =$ 9654 tons

Tons per inch immersion at summer load water line

$T =$ 36.8

Deduction = $\frac{\Delta}{40T}$ inches

= 6.56"

fresh = 167.7m

161 m/m

TABULAR FREEBOARD corrected for Flush Deck (if required)

Correction for coefficient

Depth Correction
Deduction for superstructures
Sheer correction
Round of Beam correction
Correction for Thickness of Deck amidships
Other corrections, scantlings, etc.

	+	-
Depth Correction	12.65	-
Deduction for superstructures	-	27.28
Sheer correction	-	.89
Round of Beam correction	-	.05
Correction for Thickness of Deck amidships	-	-
Other corrections, scantlings, etc.	-	-
	12.65	28.22

Summer Freeboard = 45.37

TIMBER SUMMER FREEBOARD amidships from Centre of Disc to top of Deck Line, ~~Wood~~, Steel, Deck:

Timber: Tropical Fresh Water Line above Centre of Disc 63.4

Fresh Water Line

Tropical Line

Winter Line

Winter North Atlantic Line

Summer

above

319.31

Tropical Fresh Water Freeboard ...

Fresh Water

Tropical

Winter

Winter North Atlantic

123.4

3.94 25.37 = 1152

2.9 837 834

3.3 991 985

3.34 998 985

4.5 127 127

5.34 127 127

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